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# Kinetics of low-temperature H<sub>2</sub> production in ultramafic rocks by ferroan brucite oxidation

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T = 378

20 40 60 Duration (days)

Abstract

(Inmol)

Ferroan brucite, (Mg,Fe)(OH)<sub>2</sub>, is among the potential mineral candidates for low temperature (<423 K) abiotic H<sub>2</sub> production in ultramafic rocks. To verify this assumption, synthetic ferroan brucite with grain size similar to that observed in natural samples (40–100 nm) was reacted with pure water at temperatures ranging from 348 to 573 K. Experimental products are consistent with the reaction 3 Fe(OH)<sub>2</sub><sup>brucite</sup> = Fe<sub>3</sub>O<sub>4</sub> + H<sub>2</sub> + 2 H<sub>2</sub>O. This reaction reached completion in ~2 months at 378 K and is thermally activated with an activation energy of 145 ± 1 kJ/mol. The standard state formation enthalpy and the third law entropy of amakinite, Fe(OH)<sub>2</sub>, were refined from the experimental dataset. The new thermodynamic parameters imply that ferroan brucite is stable at significantly lower hydro-

gen activity than previously calculated. The alteration of Fe-brucite produces  $H_2$  at rates compatible with present day observations of  $H_2$  emissions in natural settings (ophiolite and mid-oceanic ridges). However, efficient fluid renewal is required, as opposed to  $H_2$  production through olivine serpentinisation, which can proceed in static hydraulic conditions.

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#### Introduction

Hydrothermal circulation across upper mantle rocks at midocean ridges promotes serpentinisation reactions. In the course of these reactions, olivine reacts with water to form serpentine, magnetite and ferroan brucite, (Mg,Fe)(OH)<sub>2</sub>, along with abiotic hydrogen (Moody, 1976). As observed in ophiolites (Neal and Stanger, 1983; Abrajano *et al.*, 1990; Leong *et al.*, 2023), ultramafic rocks can still produce H<sub>2</sub> at low temperature (*i.e.* at T < 423 K), even if they are extensively serpentinised. The extrapolation of experimental kinetic data collected in the 473–623 K range (*e.g.*, McCollom *et al.*, 2016) indicates that serpentinisation of olivine with a grain size of 500 µm should reach a reaction progress above 90 % in at least 10,000 yr at temperatures below 423 K.

The serpentinisation of olivine produces secondary minerals, including ferroan brucite, which are  $Fe^{2+}$ -rich and which can further react to produce  $H_2$  + magnetite at low temperature:

$$3[Fe(OH)_2]^{brucite} = Fe_3O_4 + H_2 + 2H_2O$$
 Eq. 1

where [Fe(OH)<sub>2</sub>]<sup>brucite</sup> represents the Fe component of ferroan brucite.

Petrographic data on ophiolite and dredge seafloor samples (Jöns *et al.*, 2017; Klein *et al.*, 2020; Ellison *et al.*, 2021) seem to indicate that Reaction 1 could proceed at sub-surface conditions in partly serpentinised ultramafic rocks. H<sub>2</sub> production was achieved in hydrothermal experiments carried out

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on serpentinised peridotite at 373 K and was attributed to magnetite formation at the expense of ferroan brucite (Miller *et al.*, 2017).

In order to test the potential of Reaction 1 to produce H<sub>2</sub> at temperatures below 423 K in ultramafic rocks, the kinetics and thermodynamics of Reaction 1 were investigated experimentally here using synthetic (Mg<sub>1-x</sub>Fe<sub>x</sub>)(OH)<sub>2</sub> of grain size (40–100 nm) and composition (*x* from 0.156 to 0.205) relevant to natural ferroan brucite (Malvoisin *et al.*, 2020).

#### Materials and Methods

Ferroan brucite  $(Mg_{1-x}, Fe_x)(OH)_2$ , with *x* ranging from 0.156 to 0.205, was synthesised under ambient conditions from a stoichiometric solution of dissolved Fe(II) and Mg chlorides, as described in Carlin *et al.* (2023). The ferroan brucite obtained by this method formed platelets 40 to 100 nm across (Fig. 1a). It was loaded under an Ar atmosphere with degassed ultrapure water either in welded shut gold capsules ('caps' experiments) or in 50 mL Parr 5500 series titanium reactors ('SP' experiments; see details in Tables S-2 and S-3). The capsules were run either in horizontal cold seal pressure vessels at temperatures from 348 to 573 K at 20 MPa (caps#1 to #15) or in an oven at temperatures of 378 and 423 K at the liquid-vapour equilibrium pressure ( $P_{satr}$  caps#11 to #112). Titanium reactor experiments, SP#3 to SP#5, were conducted in the 423 to 473 K range, also at  $P_{sat}$ . SP#6 was run at 378 K with an initial Ar pressure of ~5 MPa.

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**Figure 1** Back-scattered images of (a) the starting ferroan brucite and (b–f) its reaction products. (b) Caps#9; 378 K, 2.5 days. (c, d) SP#3; 473 K, 8 days. Euhedral micrometre-sized magnetite is visible. (e) Caps#15; 573 K, 2 days. Note that ferroan brucite platelets have recrystallised. (f) SP#6; 378 K, 69 days. ~100 nm wide euhedral ferroan brucite platelets are observed. f-brc, ferroan brucite; mag, magnetite.

Pressure evolution in SP experiments was monitored at ±2 kPa with a Keller pressure sensor PA-33X. After the experiments, the H<sub>2</sub> produced and trapped in the gold capsule was sampled using the protocol described in Malvoisin et al. (2013) and analysed by gas chromatography. H<sub>2</sub> leakage through the gold capsule walls is negligible at the temperatures investigated here (Malvoisin et al., 2013). The amount of H<sub>2</sub> produced in titanium reactors was quantified either on the gas sampled at the run conditions, and/or at the end of the experiment. No H<sub>2</sub> was detected in two blank experiments performed at 378 and 473 K over more than 40 days with capsules containing only degassed ultrapure water (100 µL). Before experiments, the titanium reactors were heated to 523 K during one day in air to extract any H<sub>2</sub> potentially solubilised in the reactor wall (Louthan and Derrick, 1975), and to ensure Ti surface oxidation prior to reaction. No hydrogen production was detected in these blank experiments. Details of the sample characterisation techniques are provided in the Supplementary Information.

#### **Results and Discussion**

*Ferroan brucite oxidation reaction*. In all experiments, ferroan brucite partly decomposed into magnetite + H<sub>2</sub> (Table S-2). The H<sub>2</sub> yield increased from  $4 \times 10^{-3}$  to 220 µmol of H<sub>2</sub> *per* gram of starting material when the temperature increased from 348 to 573 K. In eight experiments (Table S-2), pyroaurite was detected (<20 wt. %), indicating the presence of minor CO<sub>2</sub> in the reacting

medium. Pyroaurite does not involve significant H<sub>2</sub> production (Carlin et al., 2023). Its impact on H<sub>2</sub> production rate is, thus, mainly associated with the lowering of the amount of ferroan brucite available for H<sub>2</sub> production. However, for experiments used for determining kinetic and thermodynamic parameters, we estimated that a maximum of 3.4 wt. % of the initial ferroan brucite was consumed to form pyroaurite. This leads to an error on the H<sub>2</sub> production rate that is small compared to the error associated with H<sub>2</sub> measurement of ~11 %. The Fe content  $(X_{\rm Fe(OH)_2})$  of ferroan brucite was determined from the refined unit cell parameters (Table S-2) based on Vegard's law (Carlin et al., 2023). It was found to vary from 0.1 to 0.2, i.e. equal or slightly below  $X_{Fe(OH)_2}$  in the ferroan brucite starting material. Recrystallisation of ferroan brucite as platelets was observed in the highest temperature experiments (Fig. 1). Unless metastable growth occurred, this observation suggests that ferroan brucite with  $X_{Fe(OH)_2} < 0.2$  is a stable reaction product in these experiments.

Altogether, the experimental results revealed that brucite partly reacted during the experiments according to Reaction 1, leading to the overall reaction:

$$(1 - x + y)Mg_{(1-x)}Fe_{x}(OH)_{2} = (1 - x)Mg_{(1-x+y)}Fe_{(x-y)}(OH)_{2}$$
$$+ \frac{y}{3}Fe_{3}O_{4} + \frac{2y}{3}H_{2}O + \frac{y}{3}H_{2}$$
Eq. 2

where *x* is the initial  $X_{\text{Fe}(\text{OH})_2}$  and *y* is a parameter related to reaction progress such as  $0 \le y \le x$ , which reflects that only a fraction, *y*/*x*, of the Fe(OH)<sub>2</sub> component in ferroan brucite has reacted. Indeed, thermodynamic equilibrium may well be achieved for *y* < *x*.

*H*<sub>2</sub> *production rate and brucite oxidation rate.* The amount of produced H<sub>2</sub> was used to retrieve the progress of Reaction 2. Magnetite was not used to infer reaction progress because, due to the presence of minor Fe<sup>3+</sup> in the starting material, part of the magnetite product may form independently of Reaction 2, i.e. without H<sub>2</sub> production (Carlin et al., 2023). The amount of H<sub>2</sub> produced in the SP experiments did not induce pressure changes significant enough to retrieve isothermal H<sub>2</sub>-production rate laws directly from pressure monitoring. However, the qualitative pressure evolution was used to determine the overall duration of the H<sub>2</sub> production stage, which, in turn, was used to model the reaction kinetics (see Supplementary Information for details). H<sub>2</sub> production kinetics at 378 K could be accurately retrieved from Run SP#6, where gas was regularly sampled (Fig. 2a). In addition, a series of experiments in gold capsules (caps#t5 to #t12) were stopped after different durations and H<sub>2</sub> was analysed in order to further constrain the kinetics of Reaction 2 (Fig. 2b). These experimental data were fitted to a kinetic law (Lasaga, 1998; see Supplementary Information for details) with the reaction rate (r) as:

$$r = r_0 \times \left(1 - \frac{Q}{K}\right)$$
 Eq. 3

where  $r_0 = k_0 \times A \times \exp(\frac{-E_a}{RT})$  with  $k_0$  a kinetic constant, A the  $Fe(OH)_2$  specific surface area,  $E_a$  the activation energy, R the gas constant and T the temperature. Q and K are the reaction quotient and the equilibrium constant of Reaction 1, respectively. The standard state is defined here with unit activity for pure minerals and water at any temperature and pressure, as well as unit fugacity for ideal gas at 1 bar of pressure and any temperature. Q was approximated to  $\frac{P_{\rm H_2}}{X_{\rm Fe(OH)_2}^3}$  with  $P_{\rm H_2}$  the H<sub>2</sub> partial pressure at the conditions of the experiment and  $X_{Fe(OH)_2}$  the molar fraction of Fe(OH)<sub>2</sub> in ferroan brucite, by assuming ideal behaviour for H2 and Fe(OH)2 in the gas phase and in the brucite solid-solution, respectively. X<sub>Fe(OH)2</sub> was calculated from Equation 2, based on the number of moles of produced H<sub>2</sub> ( $n_{\rm H_2}$ ).  $P_{\rm H_2}$  was derived from  $n_{\rm H_2}$  considering the amount of H<sub>2</sub> dissolved in the solution as calculated using PHREEQC (Parkhurst and Appelo, 2013). K was estimated with the same procedure as  $Q_{r}$  by considering that equilibrium H<sub>2</sub> pressure equals the H<sub>2</sub> partial pressure in the gas at the last measurement multiplied by a factor,  $\lambda$ , slightly above 1 (see Supplementary Information for details on this factor). Fitted  $r_0$ values are displayed in Figure 2c as a function of reciprocal temperature. The slope in the linear fit corresponds to an activation energy of 145 ± 1 kJ/mol. The intercept of the fit provides a  $k_0 \times A$ quotient of  $8.97 \times 10^7$  mol s<sup>-1</sup> g<sup>-1</sup>.

*Experimental constraints on thermodynamic properties of ferroan brucite.* Based on the kinetic law derived in the previous section, 17 experiments reached equilibrium (Table S-2). These experiments were, thus, used to constrain the equilibrium constant (*K*) of Reaction 1.

As discussed above, a set of *K* values can be calculated based on  $n_{\text{H}_2}$ , measured at the end of each experiment. A pair of  $\Delta_{\text{f}}H^\circ$  and *S*° values for the Fe(OH)<sub>2</sub> end member was retrieved by least square regression through this set of *K* values (see Supplementary Information for thermodynamic calculation details).  $\Delta_{\text{f}}H^\circ_{\text{Fe}(\text{OH})_2}$  and  $S^\circ_{\text{Fe}(\text{OH})_2}$  of  $-581.3 \pm 2.9$  kJ/mol and



**Figure 2** Kinetics of ferroan brucite alteration. **(a)** Number of moles of produced H<sub>2</sub> as a function of time at 378 K (Run SP#6; black diamonds). **(b)** Number of moles of produced H<sub>2</sub> as a function of time at 423 K (Runs caps#t5 to caps#t12; black circles). The dashed lines in **(a)** and **(b)** correspond to a fit of the data with Equation 3. **(c)**  $\ln(r_0)$  vs. 1/T. The linear regression of  $r_0$  is displayed with a black dashed line ( $R^2 = 0.87$ ) and the grey dashed lines are linear regressions for  $r_0$  with  $\lambda$  values of 1.01 and 1.20.

86.4 ± 6.3 J/mol/K were obtained, respectively. These thermodynamic values are only relevant for calculations using the same standard states as those used here, as well as the same assumption of unit activity and fugacity coefficients for ferroan brucite solid solution and H<sub>2</sub> in the gas phase, respectively. They fall in the range of published values for Fe(OH)<sub>2</sub> (Table S-4, Fig. S-3). The  $\Delta_f H^\circ_{Fe(OH)_2}$  value is consistent with the value by Ziemniak *et al.* (1995) and departs by 1.2 % from  $\Delta_f H^\circ_{Fe(OH)_2}$ , tabulated in the NIST-JANAF database (Chase, 1998). The values of the NIST-JANAF database only differ by 0.1 % from those commonly used for thermodynamic modelling of fluid–rock interactions in ultramafic rocks (McCollom and Bach, 2009). H<sub>2</sub> production prediction for our experiments is overestimated by more than one order of magnitude with the McCollom and Bach's (2009) database (Fig. S-4).

*Implications for low-T* H<sub>2</sub> *production in ultramafic systems.* Olivine serpentinisation (*e.g.*, McCollom *et al.*, 2016)





**Figure 3** Comparison of experimentally determined rate of  $H_2$  production for ferroan brucite ( $r_0$ , this study) and olivine serpentinisation (Neubeck *et al.*, 2014; McCollom and Donaldson, 2016; McCollom *et al.*, 2016). (a) Reaction rate *per* mass of starting material ( $r_0$ ). (b) Reaction rate *per* reactive surface area ( $r_0/A$ ) with A the specific surface area either measured with the BET method or calculated with the relationship provided in Brantley and Mellott (2000).

and ferroan brucite alteration (Miller et al., 2017; Ellison et al., 2021) are the two main processes that have been proposed to account for H<sub>2</sub> production at low temperature (T < 423 K) in ultramafic rocks. Excluding kinetic experiments interpreted as being distorted by artefacts (McCollom and Donaldson, 2016), a maximum of 0.028 nmol H<sub>2</sub>/g olivine/day was proposed for H<sub>2</sub> production by olivine serpentinisation at 363 K (Fig. 3a). In comparison, the rate of H<sub>2</sub> production measured here during ferroan brucite reaction  $(r_0)$  is approximately three orders of magnitude higher (Fig. 3a). When weighted by the specific surface area of the powders used in the various experiments, however, the reaction rates are rather well aligned in an Arrhenius plot with an activation energy of ~81 kJ/mol (Fig. 3b). The difference in grain sizes between olivine used in the experiments depicted in Figure 3 (38-212 µm) and the synthetic ferroan brucite used here (~50 nm) probably plays a key role in their difference of reactivity.

The respective contribution of olivine and Fe-brucite alteration to the H<sub>2</sub> production rate in natural systems was evaluated using a numerical approach. A fluid–serpentinised dunite system composed of olivine (grain size of 500  $\mu$ m; Malvoisin *et al.*, 2017), ferroan brucite (grain size of 50 nm; Malvoisin *et al.*, 2021) and water was modelled with H<sub>2</sub> being only produced by alteration of the latter minerals. A range of escape rates of H<sub>2</sub> (advection and/or diffusion) was defined in order to simulate hydrothermal activity at mid-ocean ridges, water infiltration in an ophiolitic unit or sub-stagnant hydraulic conditions in a deep aquifer. The temperature was set to 363 K, relevant to low-*T* serpentinisation (Fig. 4; see model details in Supplementary Information).

The model shows that ferroan brucite is the first mineral to react with a rate that is three orders of magnitude faster than that of olivine, leading to a rapid H<sub>2</sub> production in the first year of the reaction (Fig. 4b). In a closed system, ferroan brucite reaction rapidly stops due to the attainment of thermodynamic equilibrium (Q/K = 1). The adjustment of the thermodynamic parameters of Fe(OH)<sub>2</sub> proposed here (1.8 % and 1.2 % for  $S^{\circ}_{Fe(OH)_2}$  and  $\Delta_{\rm f} H^{\circ}_{\rm Fe(OH)_2}$ , respectively, compared to the database of McCollom and Bach, 2009) has a strong impact on the predicted equilibrium H<sub>2</sub> partial pressure and, thus, on the amount of H<sub>2</sub> that is produced. At 363 K, equilibrium is achieved for a H<sub>2</sub> molality of  $2.2 \times 10^{-5}$  mol/kg, while it is two orders of magnitude higher  $(5.0 \times 10^{-3} \text{ mol/kg})$  with the database of McCollom and Bach (2009). At 313 K, a difference of three orders of magnitude for H<sub>2</sub> molality between the two database is predicted. The oxygen fugacity ( $fO_2$ ) lies on the H<sub>2</sub>O/H<sub>2</sub>(g) equilibrium with the database of McCollom and Bach (2009) and five orders of magnitude above with the thermodynamic data derived here. Interestingly, this latter  $fO_2$  is consistent with the  $fO_2$  measured at the bottom of Holes BA1A, BA1D and BA4A during the Oman Drilling Project (Kelemen et al., 2021). After ferroan brucite reaction, olivine completely reacts in the model in approximately 3 Myr and ultimately produces 3000 times more H<sub>2</sub> than ferroan brucite (Fig. 4a).

Ferroan brucite can further react if, at the same time,  $H_2$  escapes from the system at a rate exceeding that of  $H_2$  production associated with olivine serpentinisation (Fig. 4c). This corresponds to minimum  $H_2$  escape rates of  $10^{-5}$  and  $7 \times 10^{-4}$  mol  $H_2/day/g$  rock at 313 and 363 K, respectively. The estimated



**Figure 4** Numerical modelling of the contribution of ferroan brucite alteration and olivine serpentinisation to  $H_2$  production as a function of time in a partly altered peridotite (see Supplementary Information for details). (a) General view and (b) incipient stage simulation in a closed system (no  $H_2$  leak associated with diffusion or fluid advection). (c) Simulation by considering advection of a fluid at a rate of  $1.4 \times 10^{-4}$  kg water/day/kg rock. Dashed line:  $H_2$  production associated with ferroan brucite alteration. Solid line:  $H_2$  production associated with olivine serpentinisation.

maximum escape rate by vertical diffusion is three orders of magnitude lower than this threshold value (see Supplementary Information for details), suggesting that vertical diffusion is not sufficient to drive ferroan brucite reaction. The threshold value is achieved by water renewal at a minimum rate of  $7 \times 10^{-6}$ and  $3 \times 10^{-5}$  kg water/day/kg rock at 313 and 363 K, respectively. The average water-to-rock ratio at mid-ocean ridges is ~1 (Coogan et al., 2019). Considering hydrothermal activity and fluid flow during a minimum of 30,000 yr (Früh-Green et al., 2003), it can be converted into a mean water flux of  $10^{-7}$  kg water/day/kg rock. In the Oman ophiolite, ferroan brucite with x = 0.28 can represent ~50 mol % of the serpentinisation reaction products (Malvoisin et al., 2020). Present day alteration of such ferroan brucite may occur during interaction with rainwater. H2-rich hyperalkaline fluids are found at depths >50 m (Leong et al., 2023), and the recharge rate of the aquifer in Oman is 18 mm/year (Dewandel et al., 2005). Combining these values leads to a mean meteoritic water flux of  $3 \times 10^{-7}$  kg water/day/kg rock. Both in ophiolites and on the seafloor, mean water flux estimates are, thus, approximately one order of magnitude lower than the minimum flux necessary to drive ferroan brucite reaction. However, fluid flow in ultramafic rocks is concentrated in cracks and microcracks (Dewandel et al., 2005; Corre et al., 2023) and is, thus, expected to be, locally, several orders of magnitude higher than the mean water flux. For example, the highest water-to-rock ratio values reported in abyssal peridotites are above 10<sup>5</sup> (Snow and Reisberg, 1995; Delacour et al., 2008), corresponding to water fluxes  $>10^{-2}$  kg water/day/kg rock compatible with H<sub>2</sub> production associated with ferroan brucite oxidation. The measured maximum H<sub>2</sub> production rate in the Oman ophiolite is of 71,000 mol H<sub>2</sub>/yr for a minimal volume of altered rock of 0.05 km<sup>3</sup> (Leong et al., 2023). This corresponds to a specific flux of  $10^{-3}$  nmol H<sub>2</sub>/g rock/day which is consistent with the specific H<sub>2</sub> production rate of  $5 \times 10^{-3}$  nmol H<sub>2</sub>/g rock/ day, estimated at 313 K based on the extrapolation of the data acquired here for ferroan brucite alteration (Fig. 3). Actually, the same extrapolation for serpentinisation of olivine having a grain size of 500 µm (Fig. 3b) yields a much lower production rate of  $10^{-5}$  nmol H<sub>2</sub>/g rock/day at 313 K. Ferroan brucite oxidation could thus be a main contributor to H<sub>2</sub> production at temperatures below 423 K in ophiolites and on the seafloor. This is consistent with petrographic observations in natural samples showing ferroan brucite oxidation to form magnetite in open systems conditions (Bach et al., 2006; Jöns et al., 2017).

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## Additional Information

**Supplementary Information** accompanies this letter at https://www.geochemicalperspectivesletters.org/article2408.



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